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EFFICIENCY OF GYPSIUM GRADES AND QUALITY OF LEACHING WATER FOR RECLAIMING A SALINE-SODIC SOII.

n, CHEMICAL IMPROVEMENT OF SOIL

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Gypmsum grades (5-16, 16-25, 25-60, 60-100, > 00 mesh) @ 100 %. GR of 15 cm soil column and four synthetic waters (EC 0.6 + SAR 6; E5 1.0 + SAR 12; EC 2.0 + SAR 18; EC 4.0 dS m + SAR 30), in all possible combinations, were tested for reclaiming a loamy clay saline-sodic soil in liiboratory The results experiment. indicated that the dissolation \_9.f gypsum grades varied only by less than 1 me 1 in all the synthetic waters. The reduction in EC and SAR increased as the fineness in 1: reased and/or of water decreased. The pH was decreased by coarser grades more than that tS with the finer ones, the increasing brackishness whereas of caused progressively lower decrease in pH

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## INTRODUCTION

The method for reclamation of salt-affected soils depends upon the Source and nature of soluble as *well* as exchangeable ions; *physical*, chemical and mineralogical properties; presence of lime or gypsum in *soil*, cost and the availability of both the Ca-source and irrigation water.

Being cheaper and easily available, gypsum is preferred for soil reclamation. The fineness to which gypsum must be ground is a matter of economic consideration, thoough the finer grades may ime'iove a soil ealier, Low solubility of gymsum, i.e. 25-30 me 1 (Bresler ~ al. 1982) discourages the use of

coarse particles while the excess of sodium in sodic soils favours the use of coarse grades (Keren & Shainberg, 1981).

The low hydraulic conductivity of a sodic/saline-sodic soil can be maintained or increased, irrespective of sodium saturation, by using sufficiently concentrated salt-solutions (Muhammed et al., 1969). Since most of the ground waters in the Punjab (75 % of the existing discharge of wells) are saline, saline-sodic or sodie in nature (Malik et al., 1984), it was planned to explore the possibilities to utilize these waters for leaching during reclamation of a saline-sodic soil being treated with different gypsum grades.

## MATERIALS AND METHODS

A bulk sample from surface 30 cm layer of  $t1\sim1$  Gandhra soil series (loamy clay in texture, EC = 14 dS m , SAR = 59, pH = 9.1) was collected, sun-dried, gttound and passed through a 2 Mim sieve. A 30 cm high columns each with 2400 g soil were prepared in 72 PVC\_JPipes (45 x 8.75 cm) with a uniform bulk density of 1.33 Mg m • Gypsum @ 100 % GR per 15 cm layer was mixed with the surface 15 cm before processing the pipes for uniform bulk density. This was achieved by vertically dropping the pipes four times from a height of 5 cm. The pipes were leached with 90 cm of synthetic waters under continuous submergence at 26 ± 2°C. The pipes were arranged in completely design with three replications randomized at a uniform height from floor. After the termination of the experiment, each soil column was divided into two equal depths, Le, 0-15 and 15-30 cm. These samples were analysed by the methods of the U.S. Salinity Lab. Staff (1954).

Size Limit Of Gypsum Particles

GO = No gypsum  $G_1 = 5-16 \text{ mesh};$   $G_2 = 16-25 \text{ mesh};$   $G_3 = 25-60 \text{ mesh};$   $G_4 = 60-100 \text{ mesh};$   $G_5 = > 100 \text{ mesh}.$ 

Synthetic Waters

Different synthetic waters were pepared by using NaCl,

 $\label{eq:na2S} $$Na2S\sim(j.'\ CaCI_2.2H_20$ and $MgS0_4.7H_20$ salts where $Ca:Mg::4: I, and $cr:$qfl...:: $$r:r$ ratios were $$\_rr\sim Yljained alongwith the following EC (dS m -) and SAR (rnrnol 1) levels.$ 

$$W1 = EC 0.6 + SAR 6;$$
  $W_2 = EC 1.0 + SAR 12;$   $W_3 = EC 2.0 + SAR 18;$   $W_4 = EC 4.0 + SAR 30.$ 

## RESULTS AND DISCUSSION

The dissolution of gypsum grades was determined by shaking a known weight (5g) of each grade in 100 ml of each synthetic water on a wrist action shaker for 30 minutes at 20°C. The concentration of Ca + Mg in !\text{\text{\*}}trate was recorded to be 26.43, 26.27, 26.15 and 26.06 me I, respectively in WJ, W2. W3 and W4' while that for the gypsum grades G, G2, G and ~15 was, respectively 25.94, 26.09, 26.21, 2~.36 and 310.38 me I • The differences due to synthetic water composition as well as due to size of gypsum particles were significant, though \_lthe variation in Ca + Mg concentration was less than 1 me 1 •

Soil EC<sub>e</sub>

A maxmimum significant decrease in EC occurred with W, followed by W2'  $\sim$ 3 and W4 (Table 1). R~latively higher at with W,  $\sim$ ] and  $W_4'$  though safe for most of agricultural cro~s (Mass,  $^2$ 1~ $^7$  $^7$  $^7$ , may be due to progressive higher EC + SAR of waters used for leaching. All the waters decreased EC more from the upper soil layers than from the lower ones, the eefficiency of waters remained of the same order as above. These differences appear to be due to higher water potential being useful to dissolve and carry the salts downward more from the upper than the lower layers. As the water passed through the soil, it became loaded with salts, resulting in decreased carrying power and hence less removal of salts.

The gypsum grades as well as th~lleaching alone (control) lowered the EC Ito less than 4 dS m except the GL where it was 4.16 dS  $\sim$  . However, the treatments differed satisfically and, in general, the finer gypsum grades decreased the EC more than the coarser ones. Similar results were reported by

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gypsum particles having range of size distribution (16-25 mesh) when saline-sodic water is available, can be used successfully for timely reclamation of native soils, where a variety of agricultural crops can be grown.

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